Porosity analysis of four bioceramic materials used for the repair of furcation perforations via micro-computed tomography

Hatice Yalniz^{A,D}, Fatma Gul Ziraman^{B,E}, Aysenur Oncu^{C,E}, Berkan Celikten^{E,F}

Department of Endodontics, Faculty of Dentistry, Ankara University, Turkey

- A research concept and design; B collection and/or assembly of data; C data analysis and interpretation;
- D writing the article; E critical revision of the article; F final approval of the article

Dental and Medical Problems, ISSN 1644-387X (print), ISSN 2300-9020 (online)

Dent Med Probl. 2024:61(1):71-76

Address for correspondence

Berkan Celikten

E-mail: berkancelikten@gmail.com

Funding sources

None declared

Conflict of interest

None declared

Acknowledgements

None declared

Received on July 19, 2021 Reviewed on February 1, 2022 Accepted on February 13, 2022

Published online on February 27, 2024

Abstract

Background. Porosity is a crucial parameter that affects the solubility, sealing and mechanical strength of a material. It plays a significant role in determining the success of treatment.

Objectives. The present study aimed to evaluate and compare the porosity of different bioceramic-based materials, using micro-computed tomography (micro-CT).

Material and methods. In the study, 76 permanent lower first or second molars that had been extracted for periodontal reasons and were free of calcification, resorption, root cavities, fractures, or cracks, with discrete roots and complete root apex development were selected. In each of the 4 experimental groups, perforations were made in the furcation areas of 19 molars. Mineral trioxide aggregate (MTA) Angelus®, EndoSequence® Root Repair Material (ERRM), Biodentine™, and BioAggregate were placed on the perforated areas of the samples and scanned with a micro-CT to evaluate porosity. The pore volume and the pore percentage with regard to the closed, open and total porosity of these repair materials were calculated individually in each sample.

Results. While no statistically significant differences were found between group I (MTA), group III (Biodentine) and group IV (BioAggregate) when evaluating the total pore percentage (p > 0.05), the parameter in group II (ERRM) was found to be significantly lower as compared to other groups (p > 0.05).

Conclusions. In comparison with the other materials used in this study, the use of ERRM may be more suitable for perforation repair.

Keywords: porosity, endodontics, micro-CT, tissue repair, bioceramic materials

Cite as

Yalniz H, Ziraman FG, Oncu A, Celikten B. Porosity analysis of four bioceramic materials used for the repair of furcation perforations via micro-computed tomography. *Dent Med Probl.* 2024;61(1):71–76. doi:10.17219/dmp/146663

DOI

10.17219/dmp/146663

Copyright

Copyright by Author(s)
This is an article distributed under the terms of the
Creative Commons Attribution 3.0 Unported License (CC BY 3.0)
(https://creativecommons.org/licenses/by/3.0/).

Introduction

Recently, great advances have been made in the biomedical application of ceramics for skeletal repair and reconstruction. Bioceramic materials have been used in both dental implant surgery and endodontic treatment, specifically in the repair of furcation perforations, apexogenesis, apexification, and vital pulp therapy, to induce mineralization.1 Previously, various endodontic and restorative materials, such as amalgam, glass ionomer cement (GIC), zinc oxide-eugenol cement, 2-ethoxybenzoic acid (EBA), super EBA, gutta percha, composite resin, and CavitTM, have been used for perforation repair. However, due to the lack of biocompatibility of these products and less than ideal prognosis, new materials have beeen investigated.2 Mineral trioxide aggregate (MTA) is considered the gold standard for various applications, especially as a repair material.^{3,4}

Gray ProRoot®, a calcium silicate-based MTA produced by Dentsply Maillefer (Ballaigues, Switzerland), was the only product on the market until white MTA was produced in 2002. Subsequently, new materials have been developed and compared to these 2 gold-standard MTAs. Bioceramic cements have been developed to overcome limitations, such as long hardening duration, difficulty of manipulation, discoloration of dental tissues, low radiopacity, lower compressive strength as compared to dentin, and high costs. These cements have antimicrobial properties, good impermeability and do not contain harmful heavy metals.⁵

Materials used in endodontics must ensure an impermeable cover. This is one of the most important determinants of successful root canal treatment. The durability of perforation repair is affected by the porosity of the material. The presence of closed and open pores is related to the physical properties of the material, and can have an impact on the long-term prognosis. The porosity of the material depends on its water absorption, solubility, permeability, mechanical resistance, and density. The degree of porosity is a critical factor determining its tightness.⁶ In previous studies, porosity was evaluated by measuring differences in weight before and after water absorption, using Archimedes' principle, mercury intrusion porosimetry (MIP) and micro-computed tomography (micro-CT).^{7–10} Micro-CT evnables a non-destructive

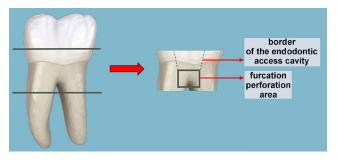


Fig. 1. Schematic pattern of the tooth/root preparation

and three-dimensional (3D) assessment of dental tissues and of the quality of the material under in vitro conditions.¹¹ Therefore, in the present study, we evaluated and compared via micro-CT the degree of porosity in the structures of 4 bioceramic-based materials – MTA Angelus®, EndoSequence® Root Repair Material (ERRM), BiodentineTM, and BioAggregate – when applied to perforation defects.

Material and methods

Specimen preparation

The study used 76 permanent lower first or second molars extracted for periodontal reasons. The teeth were free of calcification, resorption, root cavities, fractures, or cracks. They had discrete roots with complete root apex development.

The organic debris, soft tissues and calculus were meticulously removed from the teeth using the Cavitron 300 Series Ultrasonic Scaling System (Dentsply Sirona, Bensheim, Germany) and a periodontal curette (Gracey #12–14; HuFriedyGroup, Chicago, USA), without causing any damage to the root surfaces or furcation areas. To ensure disinfection, after being stored in 5% NaCl for 1 week, the teeth were kept in a physiological saline solution at ambient temperature until they were used in the study.¹²

The coronal part of the teeth was removed by making 3-millimeter cuts with diamond disks under water cooling. The apical and middle parts of the roots were then removed by cutting. Standard endodontic access cavities were created with a round diamond drill (Hager & Meisinger, Neuss, Germany) and a fissure diamond drill (Hager & Meisinger) under water cooling. The furcation areas of the obtained teeth were perforated with a 1.6-millimeter fissure drill (Hager & Meisinger). To standardize the dentine-cement thickness in the furcation area, we measured the distance between the base of the pulp chamber and the inter-radicular furcation area using a caliper. Only teeth with a thickness of 2–2.5 mm were included in the study. After washing the perforation area with a physiological saline solution, the cavities were dried with a cotton pellet and the outer surfaces of the teeth were meticulously embedded in silicone (Zetaplus C-Silicone; Zhermack, Badia Polesine, Italy), which had been placed inside a plastic cylinder to imitate the peri-radicular tissues, as in a study by Aggarwal et al.¹³ The schematic pattern of the tooth/root preparation is presented in Fig. 1.

The samples were randomly divided into 4 experimental groups of 19 specimens each (n = 19). The repair materials used were MTA Angelus (group I), ERRM (group II), Biodentine (group III), and BioAggregate (group IV).

The powder component of MTA Angelus (lot No. 45053; Angelus, Londrina, Brazil) contains tricalcium silicate, bismuth oxide, calcium carbonate, and iron oxide,

Dent Med Probl. 2024;61(1):71–76

while the liquid part is composed of water. Biodentine (lot No. B05663; Septodont, Saint-Maur-des-Fossés, France) consists of tricalcium silicate, small amounts of dicalcium silicate, calcium carbonate, and zirconium oxide. It has a water-based polymer as a liquid component, with calcium chloride, which accelerates the hardening reaction. BioAggregate (lot No. 1201BA; Innovative Bioceramix, Inc., Vancouver, Canada) consists of tricalcium silicate, dicalcium silicate, monobasic calcium phosphate, calcium hydroxide, hydroxyapatite, silica, and tantalum pentoxide. The liquid component is deionized water. EndoSequence Root Repair Material (lot No. BP11001; Brasseler USA, Savannah, USA) contains tricalcium silicate, monobasic calcium phosphate, zirconium oxide, tantalum pentoxide, and filling agents.

The material mixtures were prepared according to the manufacturers' instructions and applied to the perforated areas. To ensure hydration, the access cavities were sealed with Cavit G (3M ESPE, Seefeld, Germany) after placing moisturized cotton pellets in them. Subsequently, the samples were incubated for 72 h at 37°C in an environment with 100% humidity.

Cavit G and cotton pellets were removed from the cavities after the hardening reaction. The samples were removed from the cylinder and the silicone material on their surfaces was cleaned in preparation for micro-CT scanning.

Micro-CT scanning

The samples were enumerated and placed in a Falcon® tube, which was secured to the turntable of the micro-CT device (SkyScan 1172; Bruker, Kontich, Belgium) for high-resolution scanning. The X-ray source of the device was set to 100 kVp and 100 mA, and the samples were beamed with a rotation set at 0.40, using a 0.5-millimeter aluminum(Al)/copper (Cu) filter. Each sample was scanned while rotating 360° for 48 min. Each image was captured for 400 ms, and 3 images were taken from each angle and combined into a single image to reduce the noise ratio. Other adjustments and parameters were chosen based on the manufacturer's recommendations. Raw images were obtained from each sample, using a 10-micrometer pixel scale.

Micro-CT reconstruction and analysis of the samples

The closed pore volume, closed pore percentage, open pore volume, open pore percentage, total pore volume, and total pore percentage of the materials were assessed using micro-CT analysis.

The samples were reconstructed using the NRecon software, v. 1.6.5.2 (Bruker). The parameters for reconstruction were as follows: ring artifact 8; flattening parameter 3; and beam hardening 38%. Contrast adjust-

ments were made according to the instructions provided by the manufacturer. Overall, 1,024 two-dimensional (2D) fractions were obtained from each sample. The raw images were combined using NRecon and fractions in BMP format were obtained for internal structure analysis.

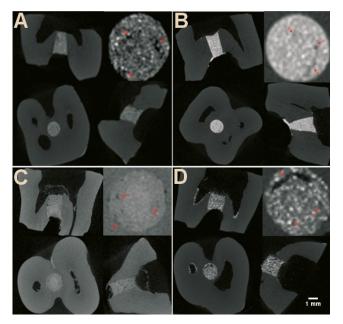


Fig. 2. Images of the coronal, transverse and sagittal planes for all experimental groups

A – group I (mineral trioxide aggregate (MTA) Angelus); B – group II (EndoSequence Root Repair Material (ERRM)); C – group III (Biodentine); and D – group IV (BioAggregate). Red arrows indicate pores in the magnified images in the upper right corner for each group.

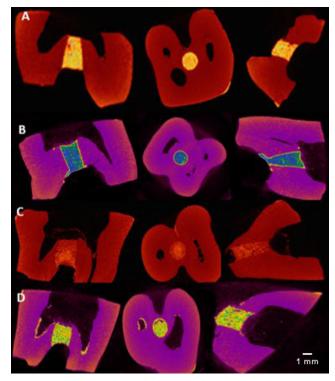


Fig. 3. Samples colored using the DataViewer software to enhance the visibility of the pores

A – group I; B – group II; C – group III; D – group IV.

These fractions were then imported into the CTAn software, v. 1.16.4.1 (Bruker), which is used to create quantitative parameters and visual models, and enables densitometric and morphometric measurements. The images were monitored in the X, Y and Z planes using the DataViewer software (Bruker) (Fig. 2,3).

Statistical analysis

The non-parametric Kruskal–Wallis test was performed due to the non-normal data distribution, which was confirmed by the Shapiro–Wilk test. Intergroup correlations were evaluated using the Mann–Whitney U test, while the Kruskal–Wallis H test with Bonferroni correction assessed intergroup differences. All analyses were conducted using the IBM SPSS Statistics for Windows software, v. 20.0 (IBM Corp., Armonk, USA), and a p-value <0.05 was considered statistically significant.

Results

Significant differences in the closed pore volume were found between group II and other experimental groups (p < 0.05), while no significant differences were observed between groups I, II and III (p > 0.05). Group II showed the lowest values for the closed pore percentage, and the differences was significant, while the highest closed pore percentage values were found in group IV, with the differences being significant (p < 0.05) (Table 1).

A statistically significant difference was found between group IV and other experimental groups regarding the open pore volume and percentage, with the BioAggregate group having the lowest values (p < 0.05) (Table 1).

Group II had the lowest values for the total pore volume, and the differences with regard to other groups were significant (p < 0.05). No statistically significant differences in the total pore volume were observed between groups I, III and IV (p > 0.05) (Table 1).

While no statistically significant differences were found between groups I, III and IV for the total pore percentage (p > 0.05), group II had the lowest total pore percentage as compared to other groups, and the differences were significant (p < 0.05) (Table 1).

Discussion

Due to the complex anatomy of the root canal, perforations may occur at the base of the pulp chamber, or on the coronal, medial or apical parts of the roots during preparation. Various materials, such as GIC, zinc oxide—eugenol cement, calcium hydroxide, and composite resins, have been used for the repair of root perforations. However, none of them have ideal features to meet the characteristics and conditions of root repair. Mercury oscillation and poor esthetics have limited the use of amalgam. Composite resins release toxic monomers and exhibit constriction during polymerization. Other materials are inadequate in terms of impermeability and coating, while having osteogenic, cementogenic and antibacterial effects. ¹⁶

Impermeable materials with high mechanical endurance should be used to repair iatrogenic furcation perforations. The use of bioceramics is considered appropriate in areas not directly related to resistance, particularly for perforation repair and pulp treatment, and in retrograde cavities to ensure hermetic obturation.¹⁷

Porosity depends on the gaps between the anhydrite cement granules, and is a natural characteristic of bioceramic-based cements. As the hydration reaction progresses, the hydration products fill the gaps, reducing porosity. However, if the water–cement ratio is too high during the mixing process, porosity increases. High liquid–powder ratios may increase porosity and solubility, and the use of a greater amount of liquid increases calcium (Ca) release from MTA.¹⁸ Moreover, the amount of air in the mixture during the mixing process and the pH of the environment also affect porosity.^{18,19}

Three different types of pores are observed: closed; through; and blind.^{20,21} Closed pores begin and end inside the material, and are therefore not related to the surface or leakage. However, they decrease the mechanical strength of the material.²² In cements, 10% porosity may reduce mechanical endurance by 50%.²³ Through pores look like tunnels that pass straight from one outer surface of the material to the other. Blind pores start at the outer surface of the material and end inside the material. Through and blind pores are related to the surface, and are called open pores. The presence of open pores negatively affects the adaptation and impermeability of the

 Table 1. Comparison of the porosity values between the experimental groups

Group	Material volume [mm³]	Closed pore volume [mm³]	Closed pore percentage [%]	Open pore volume [mm³]	Open pore percentage [%]	Total pore volume [mm³]	Total pore percentage [%]
Group I	4.421	0.251 ±0.025 ^a	5.68 ±1.23 ^a	0.226 ± 0.046^{a}	5.11 ±0.14 ^a	0.477 ±0.017 ^a	10.79 ± 1.02^{a}
Group II	4.334	0.092 ±0.015 ^b	2.12 ±0.42 ^b	0.173 ± 0.043^{a}	3.99 ± 0.04^{a}	0.265 ±0.025 ^b	6.11 ±0.96 ^b
Group III	4.525	0.342 ±0.047 ^a	7.55 ±2.27 ^a	0.248 ±0.057ª	5.48 ±0.15 ^a	0.590 ±0.062 ^a	13.04 ±2.32 ^a
Group IV	4.624	0.478 ±0.054 ^a	10.34 ±3.12 ^c	0.024 ±0.009 ^b	2.16 ±0.06 ^b	0.502 ±0.083 ^a	12.50 ±3.61 ^a

Data presented as mean \pm standard deviation (M \pm SD).

 $\hbox{Different letters in superscript show statistically significant differences between the groups.}\\$

Dent Med Probl. 2024;61(1):71–76

material.²⁴ Although porosity has a negative effect on the physical characteristics of the material, it has a positive effect on reactivity and biological characteristics by increasing the release of bioactive ions.²¹ The presence of porosity can cause microcracks in the material, and the expansion of these microcracks leads to the deterioration of the structure of the material. Such microcracks cause microleakage. Thus, the functionality of materials changes in the long run.²⁵

Gandolfi et al.¹⁰ mixed calcium silicate- and calcium hydroxide-based materials, and found that Biodentine had the highest mechanical endurance due to its low liquid–powder ratio.²⁶ Camilleri et al. reported that Biodentine was denser and less porous than MTA, but more susceptible to microorganism colonization, which negatively affected its hermetic impermeability.²⁷ Gandolfi et al. found that the porosity of MTA Angelus decreased over time due to hydraulic expansion and the formation of calcium phosphate, which closes open pores.²⁸

Porosity is directly affected by the content of the material, the liquid–powder ratio, and the problems that occur during mixing and handling.²⁹ In this study, we tested several different materials and analyzed them using micro-CT to obtain 3D, detailed and reliable data on their internal structures.³⁰ No specific data on the percentage ratios or stable levels of porosity of dental cements, obtained by micro-CT scanning, have been reported in the literature.³¹ For this reason, no control group was used in this study, and the porosity measurements of the tested materials were compared with each other.

Two studies evaluated the porosity of bioceramic-based cements. Gonçalves De Souza et al. used micro-CT to evaluate the porosity of iRoot® BP Plus, Biodentine, Ceramicrete, and ProRoot MTA.²⁹ However, they did not find any significant differences between these materials. Biodentine tended to have the lowest porosity, which was related to the trace amount of water that it contained during the mixing process.²⁹ Guerrero and Berástegui evaluated only the total porosity of the materials, and found that it was lower in Biodentine as compared to MTA.³² Silicone blocks were used in both studies. In our study, open, closed and total porosity was calculated separately to provide individual views of the leakage and mechanical endurance of the materials placed inside lower molars.

Our study revealed that ERRM demonstrated significantly lower closed pore volume and percentage as compared to MTA Angelus, Biodentine and BioAggregate. This may be attributed to the fact that ERRM consists of nanoparticles, is prepared as a paste and is easier to handle than other powder—liquid systems. BioAggregate exhibited the poorest results in terms of closed pore volume and percentage. This could be due to the larger particle size as compared to MTA Angelus and Biodentine. As suggested in previous studies, cements with larger particles tend to exhibit more in-

ternal porosity when mixed.^{27,33} Our results are in line with these findings.

On the other hand, BioAggregate showed significantly better results than MTA Angelus, ERRM and Biodentine for the open pore volume and percentage. The reason why a bioceramic-based cement would exhibit undesirable results for the closed pore volume, but desirable results for the open pore volume can be explained by the fact that materials with higher water absorption tend to expand more. Water absorption may have occurred due to the water present in the dentin tubules and the dentin barrier, rather than the water added during the mixing process. Likewise, BioAggregate shows strong adhesion to the dentin barrier, which is facilitated by humidity absorption in the dentin tubules. 34,35

The total porosity of ERRM was significantly lower as compared to other materials. When powder and liquid are added separately, and mixed afterward, air bubbles may form during the mixing process, making it harder to obtain a homogeneous mixture and leading to operator errors. EndoSequence Root Repair Material maintains its crystallized structure unless exposed to an acidic environment, absorbing water owing to its crystallized structure and forming a residue similar to hydroxyapatite. The release of calcium ions (Ca+2) reduces porosity.^{36–38}

Conclusions

For the treatment to be successful, perforation repair materials need to be durable and leak-proof. Porosity is an important physical feature of bioceramic materials. Our findings indicate that ERRM had significantly lower total porosity than the other materials tested. Within the limitations of this in vitro study, our results can promote further in vivo studies.

Ethics approval and consent to participate

Not applicable.

Data availability

The datasets generated and/or analyzed during the current study are available from the corresponding author on reasonable request.

Consent for publication

Not applicable.

ORCID iDs

References

- Best SM, Porter AE, Thian ES, Huang J. Bioceramics: Past, present and for the future. J Eur Ceram Soc. 2008;28(7):1319–1327. doi:10.1016/j.jeurceramsoc.2007.12.001
- Saxena P, Gupta SK, Newaskar V. Biocompatibility of root-end filling materials: Recent update. Restor Dent Endod. 2013;38(3):119–127. doi:10.5395/rde.2013.38.3.119
- Camilleri J, Pitt Ford TR. Mineral trioxide aggregate: A review of the constituents and biological properties of the material. *Int Endod J*. 2006;39(10):747–754. doi:10.1111/j.1365-2591.2006.01135.x
- Parirokh M, Torabinejad M. Mineral trioxide aggregate: A comprehensive literature review Part I: Chemical, physical, and antibacterial properties. *J Endod.* 2010;36(1):16–27. doi:10.1016/j. joen.2009.09.006
- Prati C, Gandolfi MG. Calcium silicate bioactive cements: Biological perspectives and clinical applications. *Dent Mater.* 2015;31(4):351–370. doi:10.1016/j.dental.2015.01.004
- De Bruyne MA, De Bruyne RJ, De Moor RJ. Capillary flow porometry to assess the seal provided by root-end filling materials in a standardized and reproducible way. *J Endod*. 2006;32(3):206–209. doi:10.1016/j.joen.2005.10.046
- Camilleri J, Grech L, Galea K, et al. Porosity and root dentine to material interface assessment of calcium silicate-based root-end filling materials. Clin Oral Investig. 2014;18(5):1437–1446. doi:10.1007/ s00784-013-1124-y
- Gandolfi MG, Siboni F, Botero T, Bossù M, Riccitiello F, Prati C. Calcium silicate and calcium hydroxide materials for pulp capping: Biointeractivity, porosity, solubility and bioactivity of current formulations. *J Appl Biomater Funct Mater*. 2015;13(1):43–60. doi:10.5301/jabfm.5000201
- Al-Fouzan K, Al-Garawi Z, Al-Hezaimi K, Javed F, Al-Shalan T, Rotstein I. Effect of acid etching on marginal adaptation of mineral trioxide aggregate to apical dentin: Microcomputed tomography and scanning electron microscopy analysis. *Int J Oral Sci.* 2012;4(4):202–207. doi:10.1038/ijos.2012.77
- Gandolfi MG, Siboni F, Primus CM, Prati C. Ion release, porosity, solubility, and bioactivity of MTA Plus tricalcium silicate. *J Endod*. 2014;40(10):1632–1637. doi:10.1016/j.joen.2014.03.025
- Bhandi S, Mashyakhy M, Abumelha AS, et al. Complete obturationcold lateral condensation vs. thermoplastic techniques: A systematic review of micro-CT studies. *Materials (Basel)*. 2021;14(14):4013. doi:10.3390/ma14144013
- Dominici JT, Eleazer PD, Clark SJ, Staat RH, Scheetz JP. Disinfection/ sterilization of extracted teeth for dental student use. *J Dent Educ*. 2001;65(11):1278–1281. doi:10.1002/j.0022-0337.2001.65.11.tb03488.x
- Aggarwal V, Singla M, Miglani S, Kohli S. Comparative evaluation of push-out bond strength of ProRoot MTA, Biodentine, and MTA Plus in furcation perforation repair. J Conserv Dent. 2013;16(5):462–465. doi:10.4103/0972-0707.117504
- Akinci L, Simsek N, Aydinbelge HA. Physical properties of MTA, BioAggregate and Biodentine in simulated conditions: A micro-CT analysis. *Dent Mater J.* 2020;39(4):601–607. doi:10.4012/dmj.2018-429
- Ma J, Shen Y, Stojicic S, Haapasalo M. Biocompatibility of two novel root repair materials. *J Endod*. 2011;37(6):793–798. doi:10.1016/j. ioen.2011.02.029
- Kakani AK, Veeramachaneni C, Majeti C, Tummala M, Khiyani L. A review on perforation repair materials. J Clin Diagn Res. 2015;9(9):ZE09–ZE13. doi:10.7860/JCDR/2015/13854.6501
- Utneja S, Nawal RR, Talwar S, Verma M. Current perspectives of bio-ceramic technology in endodontics: Calcium enriched mixture cement – review of its composition, properties and applications. *Restor Dent Endod*. 2015;40(1):1–13. doi:10.5395/rde.2015.40.1.1
- 18. Fridland M, Rosado R. Mineral trioxide aggregate (MTA) solubility and porosity with different water-to-powder ratios. *J Endod*. 2003;29(12):814–817. doi:10.1097/00004770-200312000-00007
- Coomaraswamy KS, Lumley PJ, Hofmann MP. Effect of bismuth oxide radioopacifier content on the material properties of an endodontic Portland cement-based (MTA-like) system. J Endod. 2007;33(3):295–298. doi:10.1016/j.joen.2006.11.018
- 20. Webb PA, Orr C. *Analytical Methods in Fine Particle Technology*. Norcross, GA: Micromeritics Instrument Corporation; 1997.

- 21. Camilleri J, Sorrentino F, Damidot D. Characterization of un-hydrated and hydrated BioAggregate™ and MTA Angelus™. *Clin Oral Investig.* 2015;19(3):689–698. doi:10.1007/s00784-014-1292-4
- Holt DM, Watts JD, Beeson TJ, Kirkpatrick TC, Rutledge RE. The antimicrobial effect against *Enterococcus faecalis* and the compressive strength of two types of mineral trioxide aggregate mixed with sterile water or 2% chlorhexidine liquid. *J Endod*. 2007;33(7):844–847. doi:10.1016/j.joen.2007.04.006
- Pelekanos S, Koumanou M, Koutayas SO, Zinelis S, Eliades G. Micro-CT evaluation of the marginal fit of different In-Ceram alumina copings. Eur J Esthet Dent. 2009;4(3):278–292. PMID:19704928.
- Milutinović-Nikolić AD, Medić VB, Vuković ZM. Porosity of different dental luting cements. *Dent Mater.* 2007;23(6):674–678. doi:10.1016/j.dental.2006.06.006
- De Bruyne MA, De Bruyne RJ, Rosiers L, De Moor RJ. Longitudinal study on microleakage of three root-end filling materials by the fluid transport method and by capillary flow porometry. *Int Endod* J. 2005;38(2):129–136. doi:10.1111/j.1365-2591.2004.00919.x
- Grech L, Mallia B, Camilleri J. Investigation of the physical properties of tricalcium silicate cement-based root-end filling materials. Dent Mater. 2013;29(2):e20–e28. doi:10.1016/j.dental.2012.11.007
- Camilleri J, Sorrentino F, Damidot D. Investigation of the hydration and bioactivity of radiopacified tricalcium silicate cement, Biodentine and MTA Angelus. *Dent Mater.* 2013;29(5):580–593. doi:10.1016/j.dental.2013.03.007
- Gandolfi MG, Van Landuyt K, Taddei P, Modena E, Van Meerbeek B, Prati C. Environmental scanning electron microscopy connected with energy dispersive x-ray analysis and Raman techniques to study ProRoot mineral trioxide aggregate and calcium silicate cements in wet conditions and in real time. *J Endod*. 2010;36(5):851–857. doi:10.1016/j.joen.2009.12.007
- Gonçalves De Souza ET, Nunes Tameirão MD, Roter JM, De Assis JT, De Almeida Neves A, De-Deus GA. Tridimensional quantitative porosity characterization of three set calcium silicate based repair cement for endodontic use. *Microsc Res Tech.* 2013;76(10):1093–1098. doi:10.1002/jemt.22270
- Huang Y, Orhan K, Celikten B, Orhan AI, Tufenkci P, Sevimay S. Evaluation of the sealing ability of different root canal sealers: A combined SEM and micro-CT study. J Appl Oral Sci. 2018;26:e20160584. doi:10.1590/1678-7757-2016-0584
- 31. Malkoç MA, Sevimay M, Tatar İ, Çelik HH. Micro-CT detection and characterization of porosity in luting cements. *J Prosthodont*. 2015;24(7):553–561. doi:10.1111/jopr.12251
- 32. Guerrero F, Berástegui E. Porosity analysis of MTA and Biodentine cements for use in endodontics by using micro-computed tomography. *J Clin Exp Dent*. 2018;10(3):e237–e240. doi:10.4317/jced.54688
- Camilleri J, Formosa L, Damidot D. The setting characteristics of MTA Plus in different environmental conditions. *Int Endod J.* 2013;46(9):831–840. doi:10.1111/iej.12068
- El Sayed M, Saeed M. In vitro comparative study of sealing ability of Diadent BioAggregate and other root-end filling materials. J Conserv Dent. 2012;15(3):249–252. doi:10.4103/0972-0707.97950
- 35. Leal F, De-Deus G, Brandão C, Luna AS, Fidel SR, Souza EM. Comparison of the root-end seal provided by bioceramic repair cements and White MTA. *Int Endod J.* 2011;44(7):662–668. doi:10.1111/j.1365-2591.2011.01871.x
- Batur YB, Acar G, Yalcin Y, Dindar S, Sancakli H, Erdemir U. The cytotoxic evaluation of mineral trioxide aggregate and bioaggregate in the subcutaneous connective tissue of rats. Med Oral Patol Oral Cir Bucal. 2013;18(4):e745–e751. doi:10.4317/medoral.19095
- 37. De Miranda Candeiro GT, Correia FC, Húngaro Duarte MA, Ribeiro-Siqueira DC, Gavini G. Evaluation of radiopacity, pH, release of calcium ions, and flow of a bioceramic root canal sealer. *J Endod.* 2012;38(6):842–845. doi:10.1016/j.joen.2012.02.029
- Dawood AE, Parashos P, Wong RHK, Reynolds EC, Manton DJ. Calcium silicate-based cements: Composition, properties, and clinical applications. J Investig Clin Dent. 2017;8(2). doi:10.1111/jicd.12195